

Induction motors

Types of fields (Flux)

① pulsating field

- * It has a fixed location in space
- * Its magnitude varies according to the current producing it.

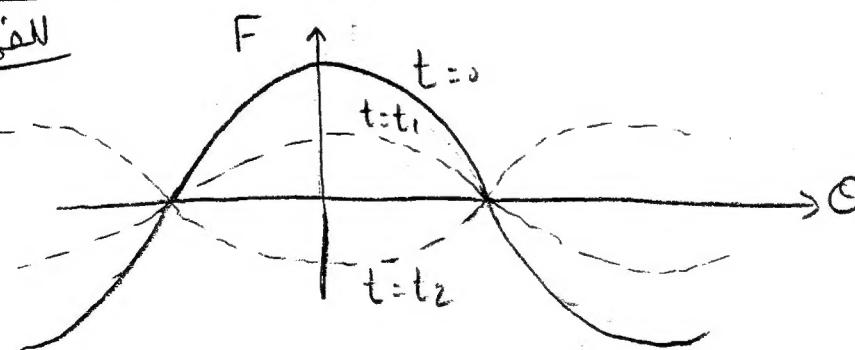
② Rotating field

- * It has constant amplitude and rotates at constant speed around periphery of the machine.

"محيط"

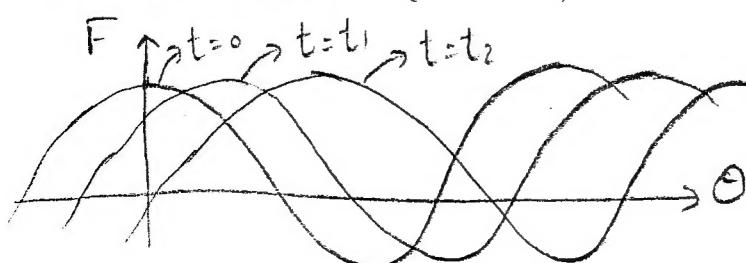
Ex: $MMF_1 = F_{max} \cos \omega t \cos \theta \Rightarrow$ pulsating

المعنى فقط



مع تغير الزمن
قيمة F تتغير لكن
مكان الpeak ثابت

$$MMF_2 = F_{max} \cos(\omega t - \theta) \Rightarrow \text{Rotating}$$



مع تغير الزمن مكان الpeak يتغير

①

Rotating field theory

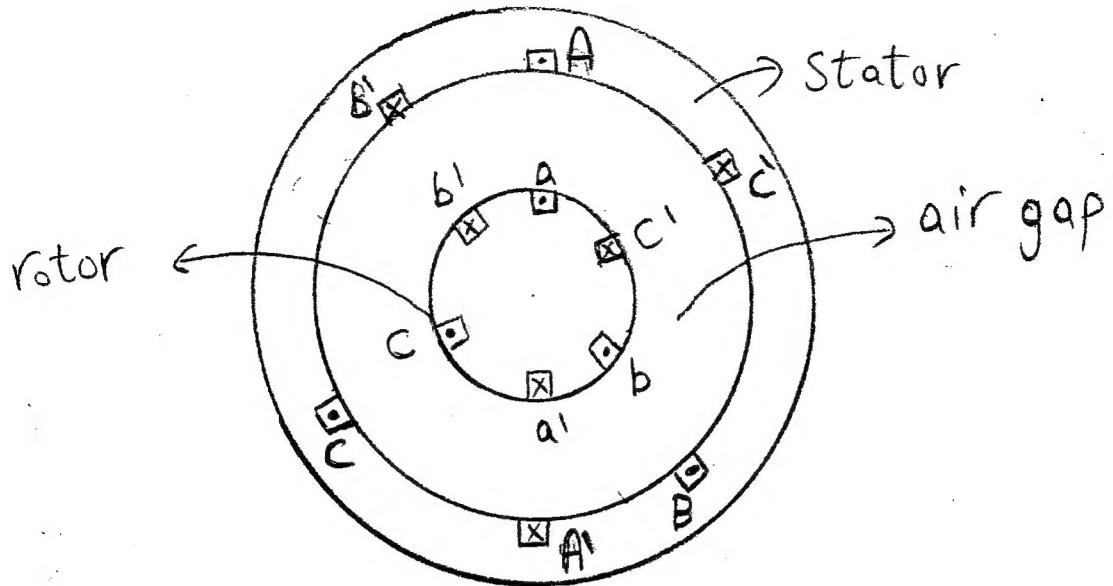
- If 3 phase balanced winding is supplied from 3 phase balanced source, then 3 phase balanced currents are produced
- Each current produce pulsating mmf (F_a, F_b, F_c)
- The resultant mmf F_{res}
$$F_{res} = F_a + F_b + F_c$$
- The resultant mmf is a rotating field which has constant magnitude & rotate with a constant speed (n_s)

$$n_s = \frac{60F}{P}$$



Where n_s : Synchronous Speed
(speed of rotating field)
 F : supply Frequency

Induction motor



Construction

It consists of

① Stator

- * 3phase winding are placed on it
- * They are shifted by 120° electrically.
- * The 3 ph: windings are supplied by 3phase balanced Ac Source
- * The stator is laminated, and have slots.

② Rotor

- * 3phase winding are placed on it
- * They are shifted by 120° electrically
- * The terminals of the 3-phase winding are short circuited.

* There are 2 types of rotors:

→ Types of rotors

① squirrel cage

- * This type of rotor is shortcircuited and has no external terminals (closed rotor), this type is commonly used.
- * Made of copper bars

② slip ring

This type has three terminals through carbon brushes & slip rings.

③ Air gap

- * The spacing between stator & rotor
- * It is used to:
 - allow rotor to rotate
 - make the machine operate in linear part in order to avoid the operation in non-linear part (saturation) of B-H curve

④

Theory of operation

3 ph balanced windings supplied from
3ph balanced Supply

3ph balanced currents in
Stator I_a, I_b, I_c

Rotating Field : (Φ_s)

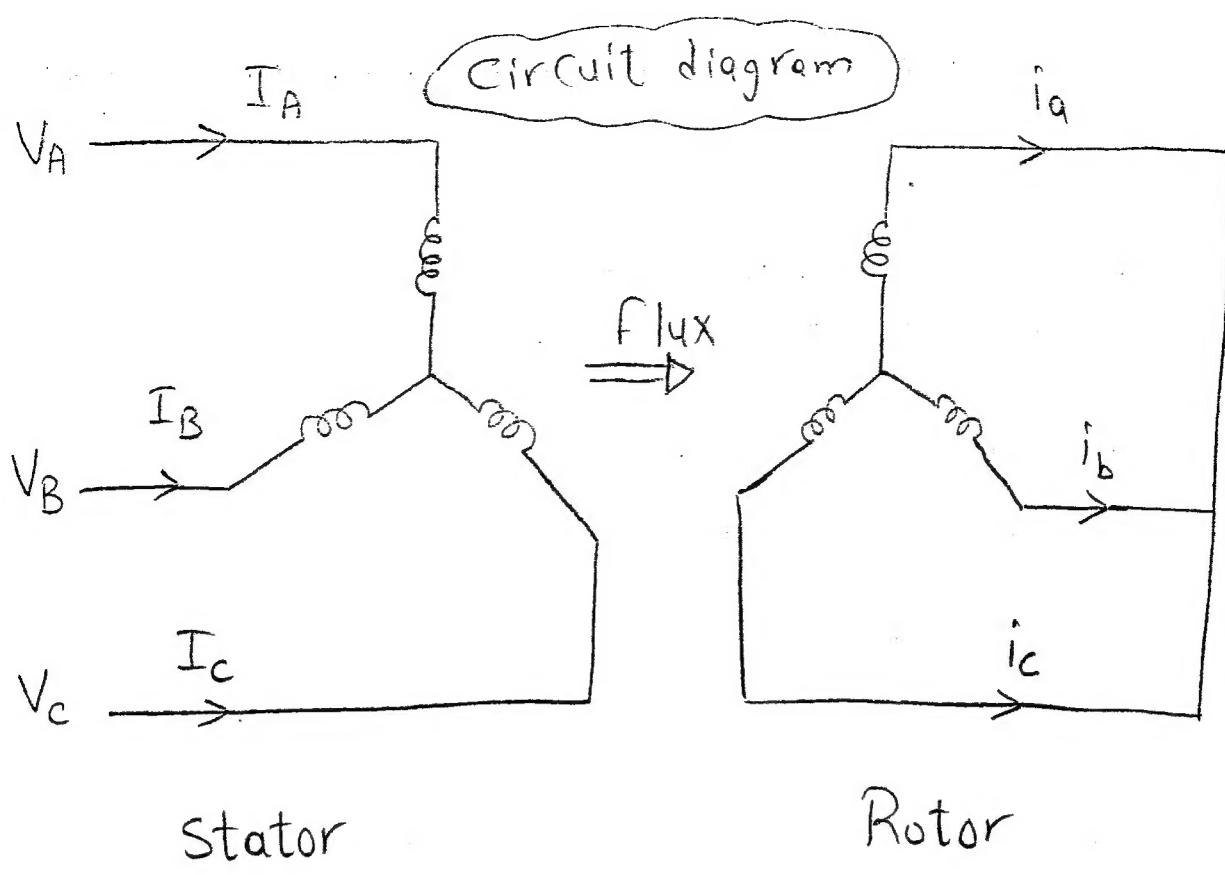
3ph induced emf's (e_a, e_b, e_c) will
be produced on rotor windings

Rotor windings are short circuited,
So 3ph balanced currents will flow
in rotor windings (i_a, i_b, i_c)

Rotating Field : (Φ_r)

The interaction between Φ_s & Φ_r
produces torque

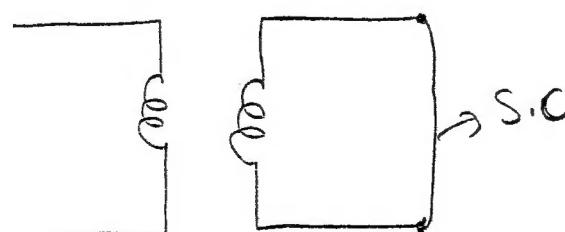
The Motor rotates



→ The theory of induction motor is similar to that of transformer. But the difference is that :

Induction motor has a rotating secondary winding, while the transformer is a static device.

→ Circuit diagram of Induction motor (1-phase)



Single phase representation (Single line diagram) (6)

Speed & Frequency in Induction motor

- * The stator field (Φ_s) & rotor field (Φ_r) rotate with the same speed (n_s)

$$n_s = \frac{60 F}{p}$$

n_s : synchronous speed

F : supply frequency

p : Number of pole pairs

- * The rotor speed is (n_r)
- * The stator speed is (Zero) [fixed body]
- * The speed of stator field or Rotor field with respect to:

$$\rightarrow \text{i) stator body} \Rightarrow n_{s-0} = n_s$$

$$\rightarrow \text{ii) Rotor body} \Rightarrow n_s - n_r$$

- * At starting (stand still), $n_r = 0$ (انہائی)∴ Speed of rotor field or stator field with respect to rotor body = n_s

Frequency of rotor current & Voltage

→ The stator flux with speed (n_s) cuts the rotor windings with speed (n_r) so the produced emf and currents have a frequency (f_r)

$$n_s - n_r = \frac{60 f_r}{P}$$

$$f_r = \frac{P}{60} (n_s - n_r)$$

$$f_r = \frac{P n_s}{60} \left(\frac{n_s - n_r}{n_s} \right)$$

$$f_r = F \left(\frac{n_s - n_r}{n_s} \right)$$

Let $s = \frac{n_s - n_r}{n_s} \Rightarrow$ slip

$$\therefore f_r = s F$$

$$f_r \ll F$$

Where: f_r : Frequency of emf & current induced in rotor

F : Supply frequency

s : slip (It represents difference between stator field speed & rotor body speed) (8)

Speed laws

RL

$$① n_s = \frac{60F}{P}$$

- n_s : Synchronous speed
- F : Supply Frequency (usually 50 or 60 Hz)
- P : Number of pole pairs.
- $2P$: Number of poles

$$② S = \frac{n_s - n_r}{n_s}$$

- S : Slip
- n_r : Rotor speed or motor speed

$$③ f_r = SF$$

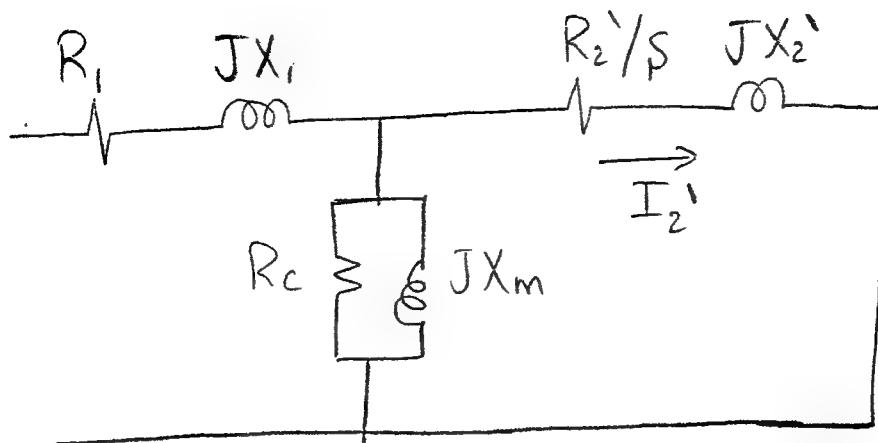
- f_r : Frequency of emf's induced in rotor winding
- F : Supply frequency

④ * Speed of stator field & rotor field is n_s

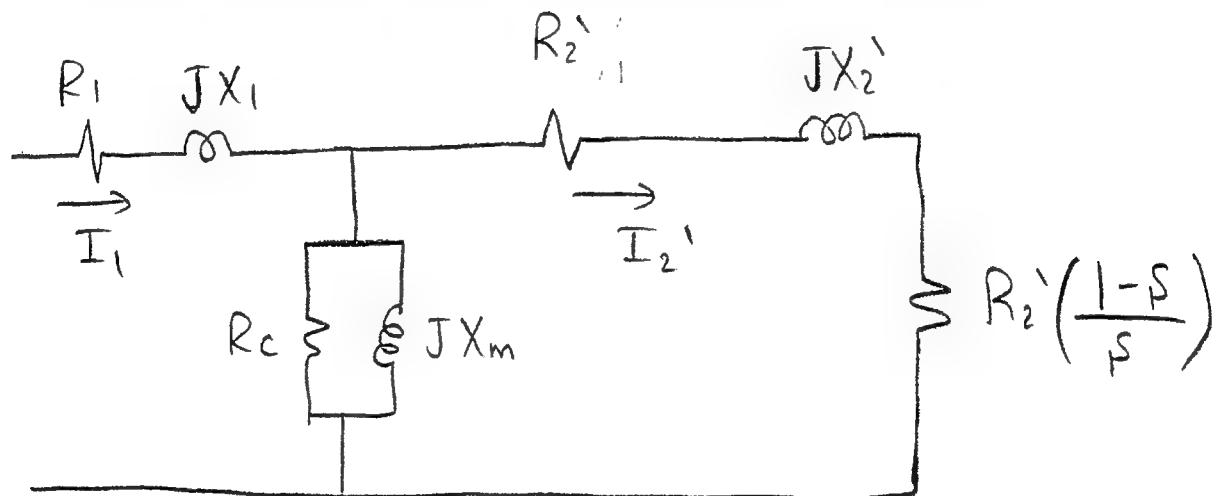
* Speed of stator field or rotor field relative to rotor is $n_s - n_r$

Equivalent circuit of induction motor

"مخطط قوى ينبع من المبدأ"



Induction motor \equiv Transformer with S.C load



R_2' : Rotor resistance referred to stator

I_2' : Rotor current referred to stator

Types of power loss in induction motor

① Stator Copper loss ($P_{Cu\text{stator}}$)

Due to resistance of stator winding

② Stator Core loss (P_{core})

Due to iron losses in stator core
(eddy losses)

③ Rotor Copper loss ($P_{Cu\text{rotor}}$)

Due to resistance of rotor winding

④ Mechanical (rotational) losses

Due to friction that opposes the moving rotor.

Important note



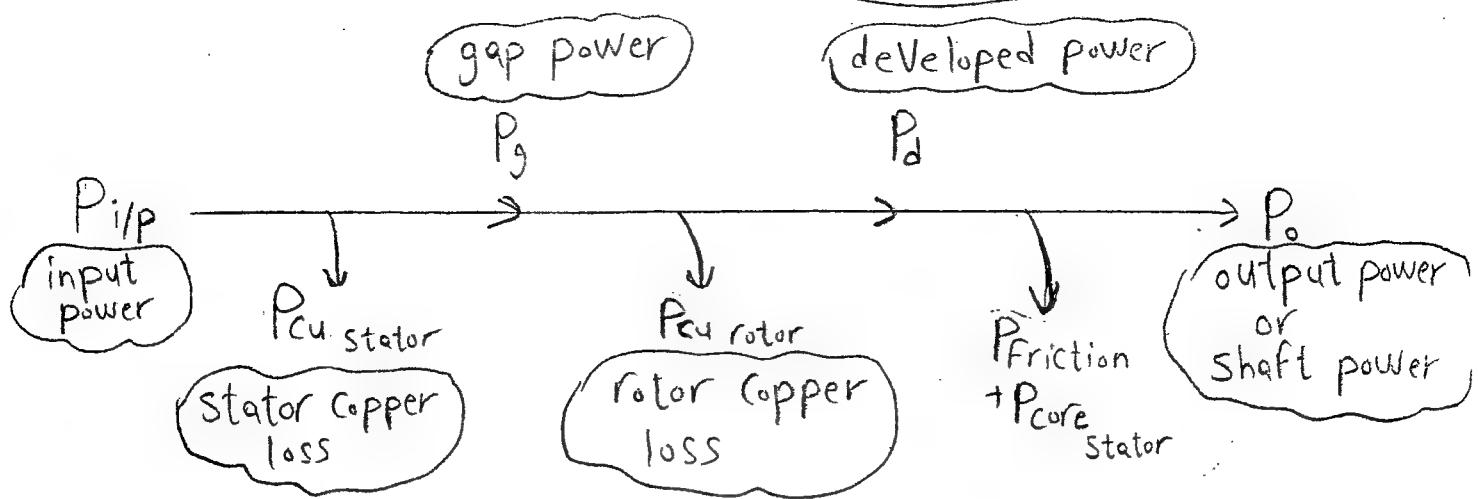
Rotor Core loss is neglected because

$$P_{core\text{rotor}} = P_{er\text{rotor}} + P_{h\text{rotor}}$$

$$* P_{eddy\text{rotor}} \propto F_r^2 \quad * P_{hysteresis\text{rotor}} \propto F_r$$

But $F_r = SF$ ($F_r \downarrow \downarrow$) $\Rightarrow P_{core\text{rotor}}$ is neglected.

power flow in induction motor



$$* P_g = P_{i/p} - P_{Cu \text{ stator}}$$

$$* P_o = P_d - (P_{Friction} + P_{core \text{ stator}})$$

$$* P_{i/p} = \sqrt{3} V_{L_L} I_{L_L} \cos \phi$$

$$* P_{Cu \text{ stator}} = 3 I_s^2 R_s$$

$$* P_g = \frac{3 I_r^2 R_r}{s} = \frac{3 I_r^2 R_r}{s}$$

$$* P_{Cu \text{ rotor}} = 3 I_r^2 R_r' = 3 I_r^2 R_r$$

$$* P_d = 3 I_r^2 R_r \left(\frac{1-s}{s} \right) = 3 I_r^2 R_r \left(\frac{1-s}{s} \right)$$

$$* P_d = (1-s) P_g$$

$$P_g = \frac{P_{Cu \text{ rotor}}}{s}$$

$$* P_o = P_i - P_{c\text{u}stator} - P_{c\text{u}rotor} - P_{\text{friction}} - P_{\text{core}}$$

$$* \eta = \frac{P_o}{P_i}$$

$$\eta = \frac{P_o}{P_o + P_{c\text{u}stator} + P_{c\text{u}rotor} + P_{\text{friction}} + P_{\text{core}}}$$

Note:

- P_g is called gap power or power input to the rotor

IF Torque is required

$$\rightarrow T_d = \frac{P_d}{\omega_r} = \frac{P_g(1-s)}{\omega_s(1-s)} = \frac{P_g}{\omega_s}$$

$\rightarrow T_d$: electromagnetic developed Torque

$$* \omega_s = \frac{2\pi n_s}{60}$$

$$\rightarrow T_{\text{shaft}} = \frac{P_{\text{shaft}}}{\omega_r} = \frac{P_o}{\omega_r}$$

(13)

Pb 7

- * 3 phase Induction motor, 60Hz
- * Shaft power = 80kW ($P_o = 80\text{ kW}$)
- * $P_{\text{friction}} = 920\text{ W}$, $P_{\text{core}} = 4300\text{ W}$, $P_{\text{Cu}} = 2690\text{ W}$
stator stator
- * $I_r' = 110\text{ A}$, $R_r' = 0.15\Omega$, $S = 3.8\%$.

Required \Rightarrow Find η

Solution

$$\rightarrow P_{\text{Cu, rotor}} = 3(I_r')^2 R_r' = 3(110)^2 (0.15\Omega)$$

$$P_{\text{Cu, rotor}} = 5.445\text{ kW}$$

$$\begin{aligned}\rightarrow P_i/p &= P_o + P_{\text{Cu, stator}} + P_{\text{Cu, rotor}} + P_{\text{friction}} + P_{\text{core}} \\ &= 80 + 2.69 + 5.445 + 0.92 + 4.3 \\ &= 93.35\text{ kW}\end{aligned}$$

$$\rightarrow \eta = \frac{P_o}{P_i} = \frac{80}{93.35} = 85.7\%$$

$$\eta = 85.7\%$$

pb. ⑧

- 3-ph I.M, 50Hz, 6 poles
- $P_i = 40 \text{ kW}$
- $n_r = 975 \text{ rpm}$
- $P_{\text{copper stator loss}} = 1 \text{ kW} / (P_i)$
- $P_{\text{friction}} = 2 \text{ kW}$

Required: Find

i) Slip ii) P_{BCL} iii) P_d iv) η

Solution

$$n_s = \frac{60F}{P} = \frac{60 \times 50}{3} = 1000 \text{ rpm}$$

i) Slip

$$S = \frac{n_s - n_r}{n_s} = \frac{1000 - 975}{1000} = 0.025$$

$$S = 0.025$$

ii) P_{RCL}

$$* P_g = P_i - P_{Cu\text{stator}}$$

$$P_g = 40 - 1 = 39 \text{ kW}$$

$$* P_{RCL} = S P_g = 0.025 * 39$$

$$P_{RCL} = 0.975 \text{ kW}$$

iii) P_d

$$P_d = (1-S) P_g = (1-0.025) * 39$$

$$P_d = 38.025 \text{ kW}$$

$$\text{or } P_d = P_g - P_{RCL} = 38.025 \text{ kW}$$

iv) η

$$\Rightarrow P_o = P_d - P_{\text{friction}} = 38.025 - 2 = 36.025 \text{ kW}$$

$$\Rightarrow P_i = 40 \text{ kW}$$

$$\eta = \frac{P_o}{P_i} = 90.06\%$$

$$\eta = 90.06\%$$

Pb. 9

- 3ph I.M., 50Hz, 6 poles
- power input to the rotor (P_g) = 80kW
- Rotor emf makes 100 alternations (cycles) per minute

Find

(i) Slip (ii) Motor speed (nr) (iii) P_a

Solution

$$\textcircled{i} \quad f_r = 100 \frac{\text{Cycle}}{\text{min}} = 100 \frac{\text{Cycle}}{60 \text{ sec}} = 1.667 \text{ Hz}$$

$$\text{but } f_r = SF$$

$$\therefore S = \frac{f_r}{f} = \frac{1.667}{50} = 0.033$$

$$\therefore \textcircled{S = 0.033}$$

$$\textcircled{ii} \quad S = \frac{n_s - n_r}{n_s}$$

$$\text{but } n_s = \frac{120f}{P} = \frac{120(50)}{6} = 1000 \text{ rpm}$$

$$\therefore 0.033 = \frac{1000 - n_r}{1000} \Rightarrow \textcircled{n_r = 967 \text{ rpm}}$$

iii) $P_d = (1-s) P_g$

$\therefore P_d = (1-0.033) * 80$

$\therefore P_d = 77.36 \text{ kW}$

Pb. 10

• 3 ph I.M, 50Hz, 4 poles, $s = 0.05$

• Find the speed of rotor mmf (flux) relative to the rotor

Solution

$$\Rightarrow \text{Speed of rotor m.m.f} = n_s = \frac{120F}{P} = 1500 \text{ rpm}$$

$$\Rightarrow \text{Speed of rotor body} = n_r = (1-s)n_s = 1425 \text{ rpm}$$

• Speed of rotor m.m.f relative to rotor

$$\text{body} = n_s - n_r = \boxed{75 \text{ rpm}}$$

Ex: A 3phase, 2 poles, 60HZ induction motor operates at a speed of 3502 rpm with an input power of 15.3KW and terminal current of 22.6A. Stator winding resistance $R_s = 0.2\Omega/\text{phase}$

calculate : ① air gap power
 ② Rotor Copper loss

Solution

Terminal current = stator current

$$\textcircled{1} \quad P_g = P_{i/p} - P_{Cu \text{ stator}}$$

$$* P_{i/p} = 15.3\text{KW}$$

$$* P_{Cu \text{ stator}} = 3I_s^2 R_s = 3(22.6)^2(0.2) = 0.306\text{KW}$$

$$\therefore P_g = 15.3 - 0.306 \Rightarrow \textcircled{P_g = 14.994\text{KW}}$$

$$\textcircled{2} \quad P_{Cu \text{ rotor}} = s P_g$$

$$s = \frac{n_s - n_r}{n_s}$$

(19)

$$n_s = \frac{60F}{P} = \frac{60(60)}{1} = 3600$$

$$\therefore S = \frac{n_s - n_r}{n_s} = \frac{3600 - 3502}{3600} = 0.0272$$

$$\therefore P_{cur, \text{rotor}} = SP_g = (0.0272)(14.994)$$

$$P_{cur, \text{rotor}} = 407.8 \text{ W}$$



- 1- Why is the stator core of Alternator laminated?
- ✓ 2- What are the losses in the 'induction motor' and briefly explain them?
- 3- In a 3-phase synchronous motor
 - (A) the speed of stator MMF is always more than that of rotor MMF.
 - (B) the speed of stator MMF is always less than that of rotor MMF.
 - (C) rotor and stator MMF are stationary with respect to each other.
- 4- Why almost all large size Synchronous machines are constructed with rotating field system type?
- 5- Why are Alternators rated in kVA and not in kW?
- 6- Write down the equation for frequency of emf induced in an Alternator.
- ✓ 7- The shaft output of a three-phase 60- Hz induction motor is 80 KW. The friction and windage losses are 920 W, the stator core loss is 4300 W and the stator copper loss is 2690 W. The rotor current and rotor resistance referred to stator are respectively 110 A and 0.15 Ω . If the slip is 3.8%, what is the percent efficiency?
- ✓ 8- The power input to a 500 V, 50 Hz, 6 pole 3 phase squirrel cage induction motor running at 975 rpm is 40 KW. The stator losses are 1 KW and the friction and windage losses are 2 KW. Calculate
 - (i) Slip (ii) Rotor copper loss
 - (iii) Mechanical power developed (iv) The efficiency.
- ✓ 9- The power input to the rotor of a 3-phase, 50 Hz, 6 Pole induction motor is 80 kW. The rotor emf makes 100 complete alternations per minute. Find
 - (i) the slip (ii) the motor speed and (iii) the mechanical power developed by the motor.
- ✓ 10- A balanced three-phase, 50 Hz voltage is applied to a 3 phase, 4 pole, induction motor. When the motor is delivering rated output, the slip is found to be 0.05. The speed of the rotor m.m.f. relative to the rotor structure is:
 - (A) 1500 r.p.m. (B) 1425 r.p.m.
 - (C) 25 r.p.m. (D) 75 r.p.m.
- 11- A three-phase, 500 MVA 20.8 kV four-pole star-connected synchronous machine has negligible stator resistance and a synchronous reactance of 0.8 Ohm per phase at rated terminal voltage. The machine is operated as a generator connected to a three-phase 20.8 kV infinite bus.
Note: 20.8 kV is the line voltage.
a Give the per-phase equivalent circuit of the synchronous machine.
b Calculate the phase voltage.
c Sketch the phasor diagram when the machine is delivering rated MVA at a power factor of 0.8 lagging.



Synchronous and Induction Machines
 Dynamic Equations

d Determine the excitation voltage and the power angle when the machine is delivering rated MVA at a power factor of 0.8 lagging.

12- For the system of Fig.1 the magnetic force is opposed by the inertial force, damping force and the spring force. Write down the force balance equation where:

c is the spring constant proportional to the displacement, b is the damping coefficient proportional to the velocity and m is the mass of the system.

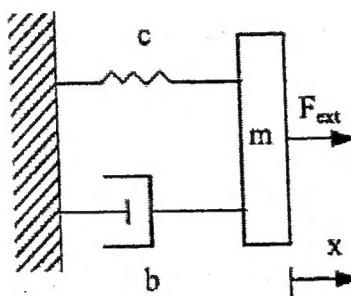


Fig.1: Mechanical system, Spring-Mass-Damper

13- Derive the electrical and mechanical equations of motion of the mechanical system shown in Fig.2.

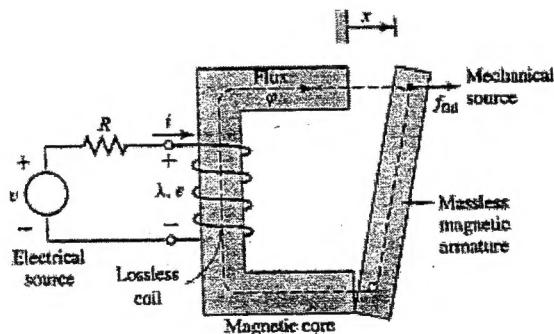


Fig.2: Electromechanical system